

An LCD tachistoscope with submillisecond precision

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Abstract Tachistoscopes allow brief visual stimulation delivery, which is crucial for experiments in which subliminal presentation is required. Up to now, tachistoscopes have had shortcomings with respect to timing accuracy, reliability, and flexibility of use. Here, we present a new and inexpensive two-channel tachistoscope that allows for exposure durations in the submillisecond range with an extremely high timing accuracy. The tachistoscope consists of two standard liquid-crystal display (LCD) monitors of the light-emitting diode (LED) backlight type, a semipermeable mirror, a mounting rack, and an experimental personal computer (PC). The monitors have been modified to provide external access to the LED backlights, which are controlled by the PC via the standard parallel port. Photodiode measurements confirmed reliable operation of the tachistoscope and revealed switching times of $3\ \mu\text{s}$. Our method may also be of great advantage in single-monitor setups, in which it allows for manipulating the stimulus timing with submillisecond precision in many experimental situations. Where this is not applicable, the monitor can be operated in standard mode by disabling the external backlight control instantaneously.

Keywords Visual perception · Tachistoscope · Subliminal stimulation · LCD · LED backlight · Visual stimulation device

Traditional mechanical and electrical tachistoscopes are cumbersome to use and have limitations primarily due to their physical components, particularly when brief exposure durations are used (see, e.g., Lancaster & Lomas, 1977; Mollon & Polden, 1978). Electrical tachistoscopes use fluorescent lamps working as shutter components to passively illuminate images consisting of handmade photo prints presented via manual slide-projection systems (e.g., Karlin, 1955; Kupperian & Golin, 1951). These lamps exhibit rather slow and variable response times (up to 20 ms), creating noise and imprecise timing (e.g., Bohlander, 1979; Glaser, 1988; Merikle, 1980; Mollon & Polden, 1978). Tachistoscopes using mechanical shutters (e.g., Deutsch, 1960; Lancaster, Sayer, Scott, & Sutcliffe, 1971) are often failure-prone, with variable asymmetries in rise and fall times of the order of several milliseconds (e.g., Madigan & Johnson, 1991; Naish, 1979).

Presenting complex visual stimuli at ultrashort durations—that is, within the submillisecond range—as opposed to simple flashes of light (e.g., Efron, 1964) in a controlled and efficient manner has not been achieved yet with standard screens and projectors (Bukhari & Kurylo, 2008; Krantz, 2000; Wiens et al., 2004; Wiens & Öhman, 2005). Recently, tachistoscopes have been described that are based on data projectors and liquid-crystal (LC) shutters (Fischmeister et al., 2010) or on LC panels with light-emitting diode (LED) arrays (Thurgood, Patterson, Simpson, & Whitfield, 2010). Although these setups provide millisecond resolution, they rely heavily on expensive or custom-made components.

Here, we present a simple and inexpensive alternative for displaying images with a high presentation quality and timing, at exposure durations starting in the submillisecond range. Our tachistoscope is based on two liquid-crystal display (LCD) monitors of the LED backlight type, which are set around a semipermeable mirror. Both monitors are aligned so as to appear at the same position when viewed through the mirror. As compared

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to a slide projector tachistoscope with mechanical shutters, the LC panel plays the role of the slide, and the LED backlight the role of the shutter and the projector. While the backlight is off (shutter closed), the image can be changed on the LC panel without being visible to the observer. Once the image has been transmitted to the LC panel and the LC pixel cells have settled to a steady state, the backlight can be switched on (shutter open) to instantly make the image visible.

Method and materials

LCD monitors

We first explain the working principle of an LCD, as this information is closely related to how our tachistoscope operates. An LCD consists of a white backlight that illuminates, from behind, an array of LC pixel cells. These pixel cells serve as light valves whose transmission factors can be programmed individually. A colored filter is present in front of each pixel cell, only letting red, green, or blue light pass. A single image pixel is formed by three such pixels (red, green, and blue). The LC pixel cells and the colored filters are mechanically sealed and are here referred to as *LC panel*. The LC panel works independently of the backlight.

The backlight, which does not have a pixel structure, illuminates all of the pixels of the LC panel at once, even when a black screen is presented.¹ The brightness of the backlight can be controlled by the user through the monitor settings (usually the brightness control). The monitor electronics actually vary the brightness by digitally switching the backlight on and off repeatedly at a frequency of around 200 Hz. The on–off ratio determines the average brightness. This principle is called *pulse width modulation* (PWM) and is exactly what is used in our tachistoscope application, apart from that the frequency and on–off ratio take rather extreme values. This PWM principle is not only used with LED backlights, but also with cold cathode fluorescence lamp (CCFL) backlights. However, the switching characteristics of LEDs are what make LED backlights the technology of choice for the tachistoscope application.

In a standard LCD monitor, the pixel values in the LC panel are the only parameters that change over time and under computer control. This is a rather slow process, for two reasons. First, if a pixel cell has received a new value, it needs some time to settle to this new value. This time is characterized by the so-called *reaction time*. Second, the pixel array cannot be programmed at once, but is updated pixel-wise, from the top left of the screen to the bottom

right. Once a pixel has received a new value, it autonomously keeps its value until the next update or refresh cycle. This update process is usually visible, at least in a physical sense, because the LC panel is illuminated by the backlight at all times. In our tachistoscope application this is different, as the backlight can be switched off during the update process and be switched on again at any time after all of the pixel cells have sufficiently settled to their new values.²

Tachistoscope

We used two LCD monitors (Samsung SyncMaster BX2240) to create the images for visual stimulation (for comments regarding monitor selection, see [Appendix A](#)). The monitors are situated around a semipermeable mirror (Glas Trösch 50:50 Luxar beam splitter), such that the observer perceives the images of both monitors superimposed (Fig. 1). The monitors are directly connected to a graphics card with two graphics outputs. Moreover, the LCD control electronics were modified to allow an external device to take over the control of the LED backlight, in order to switch it on or off. We controlled the backlight via the parallel port of the stimulus PC.³

As compared to a traditional tachistoscope based on slide projectors, the LC panel plays the role of the slide, whereas the LED backlight plays the role of either a switchable light bulb or a mechanical shutter. As the slow changing of the slide in a traditional tachistoscope is hidden by the faster switching shutter, the relatively slow changing of the pixel states in the LC panel is hidden by the fast-switching LED backlight. Switching the LED backlight can be precisely timed and takes just a few microseconds, whereas switching traditional mechanical shutters or LC shutters takes a few milliseconds. Moreover, the switching characteristics are almost identical for both switching directions (i.e., on–off and off–on), thereby minimizing the period during which there is uncertainty about which of the images is being displayed. Having two monitors (i.e., two channels) allows for presenting a stimulus over or embedded in an arbitrary background.

The timing of a briefly flashed stimulus on a background is illustrated in Fig. 2. Noteworthy, as the LED backlights of the two monitors can not only be switched in a complementary manner, but also on or off for both monitors, other stimulus sequences are possible as well. For example, presenting a stimulus and a mask over a black background is possible, with hardly any limitations regarding the timing.

² This description of LCD monitors refers to standard consumer products and cannot be accurate for all different types and variations of LCD monitors.

³ We used MATLAB (The MathWorks, Natick, MA) with the Psychophysics Toolbox extensions (Brainard, 1997) to program the device.

¹ This is not true when special techniques are applied, including dynamic contrast, flashed backlight, scanning backlight, and so forth.

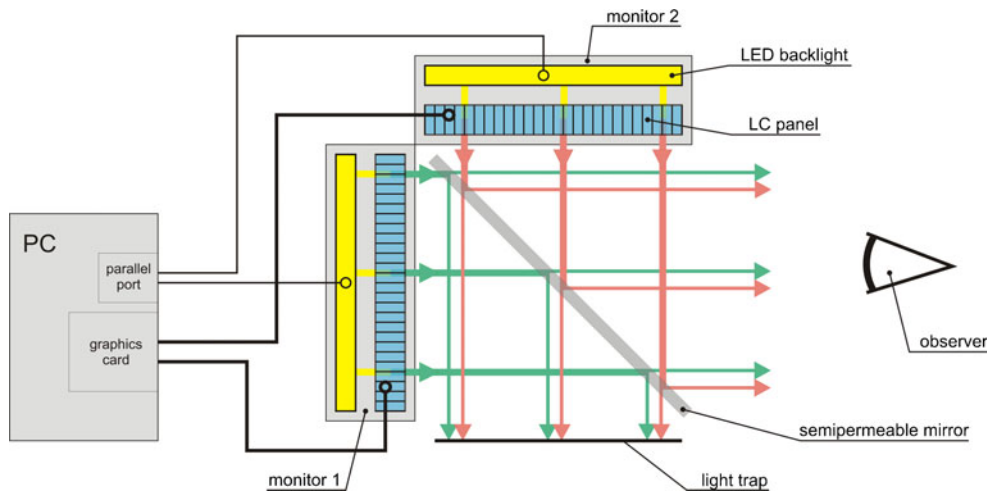


Fig. 1 Each monitor has a light-emitting diode (LED) backlight (yellow), which can be instantly switched on or off for the complete screen. The light is modulated by the liquid-crystal (LC) panel (blue), which, in contrast to the backlight, has a pixel structure and reacts rather slowly when the pixel values are changed. The image is only visible when the backlight is switched on, because the single-pixel cells in the LC panel work like programmable light valves that just modulate the

light coming from the backlight but are not light sources themselves. The light output of each monitor (illustrated as green beams for Monitor 1 and red beams for Monitor 2) is split by a 50:50 semipermeable mirror. One output path of the semipermeable mirror is absorbed by a light trap (e.g., black cardboard), while the other can be observed. For the observer, Monitor 2 appears to be at exactly the same position as Monitor 1

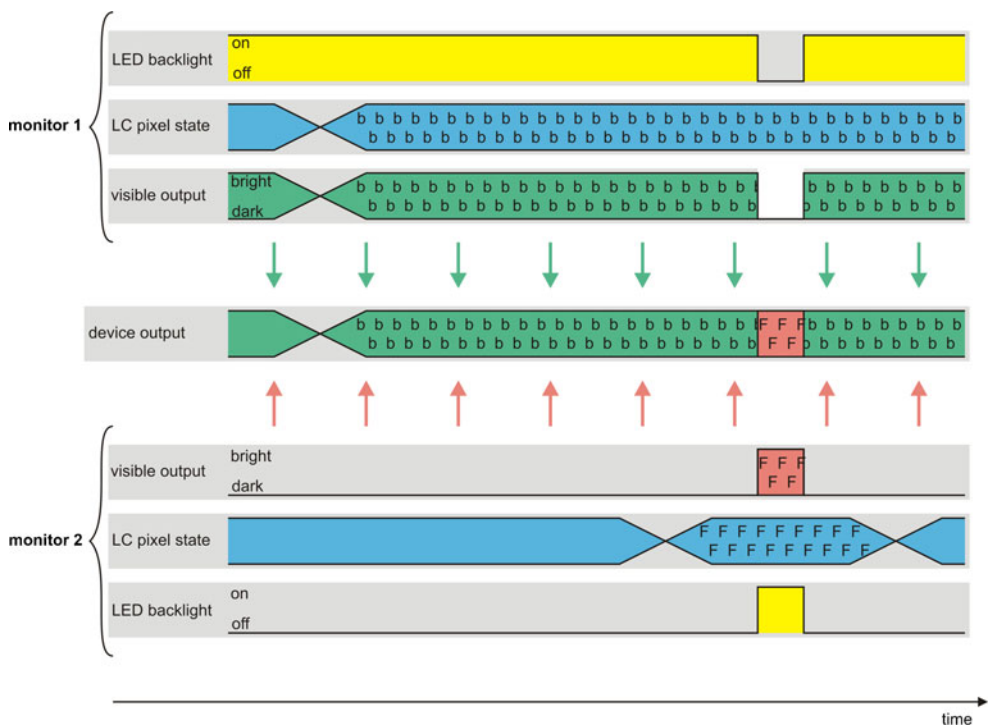


Fig. 2 Timing example for the control signals and the respective light outputs of the two-channel tachistoscope for a briefly flashed stimulus. The state of the LC panel (shown in blue) is controlled by the graphics card, and each pixel has an individual color and luminance. The image is only visible while the LED backlight (shown in yellow) is switched on. The light outputs (shown in green for Monitor 1 and in red for Monitor 2) are combined by the semipermeable mirror and form the output seen by the observer (signal in the middle of the figure). The first image switch occurs for Monitor 1 while the LED backlight is on

(with the new image marked “b” for background), resulting in the normal LCD behavior, with a rather slow transition from the previous image to the new one. Then the image for Monitor 2 is changed (“F” for foreground), but this transition is not visible because the LED backlight is off. When everything has settled, the backlights of both monitors are switched synchronously for a short period of time (pulse), causing a switch of the visible image in the output, with transition times being determined solely by the switching times of the LEDs—that is, basically instantly

LED backlight control

Each of the two monitors needed to be internally modified in order to permit control of the LED backlight by an external source. In the simplest case, this is a matter of identifying the signal line carrying the PWM signal to the LED driver, disrupting it from the internal source, and making it available to an external source. We added an optional small circuit, which served two purposes. First, it performed a voltage level translation from 3.3 V, at the computer's parallel port, to 5 V, used in the monitor.⁴ Second, the circuit allowed for switching the monitor between external backlight control—that is, tachistoscope mode—and internal standard PWM mode (Fig. 3).

Program timing

In a typical tachistoscope application, the computer program updates the image while the backlight of the monitor is switched off. The updating time of the image depends on several factors, such as the graphics programming mode (e.g., single vs. double buffered) and the image data processing within the monitor. Most importantly, the image data is transmitted in a pixel-sequential manner, not only when the data is transmitted to the monitor, but also when the data is transmitted within the monitor to the LC panel. Hence, pixels at the top of the screen are updated first, whereas pixels at the bottom are updated last, almost one refresh cycle later (Fig. 4). Finally, once an LC pixel has been updated to a new value, time is needed for the pixel to settle to this new value. The amount of time required depends on the difference between the old and new pixel values, the monitor's contrast setting (see also LCD Reaction Time, in the Measurements section below), and the acceptable pixel luminance error.

Here is an example of typical program timing. After the value of a particular pixel P has been altered by the program via the graphics command, it takes one refresh cycle, at maximum, until the new pixel value is processed by the output stage of the graphics card and transmitted to the monitor (16.7 ms, assuming a monitor refresh frequency of 60 Hz). If the monitor does not perform any time-consuming image data processing, the corresponding LC pixel P will be updated at the same time that the value for pixel P arrives at the monitor. Assuming that the LC pixel maximally needs 50 ms to settle to the new value within an acceptable error range, the program must not switch on the LED backlight earlier than $16.7 + 50 \text{ ms} \approx 67 \text{ ms}$ after having issued the last graphics command. Otherwise, the luminance of the presented pixels might be inaccurate.

⁴ Some parallel-port implementations work with a logic high level of 3.3 V, at least for the data lines. Others work with 5 V.

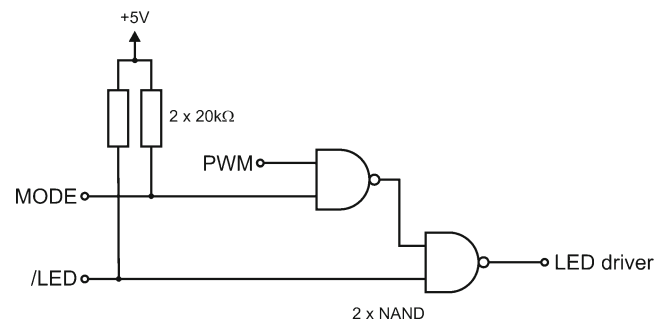


Fig. 3 Multiplexer circuit that allows selecting between the internal PWM and the external /LED control signal. The internal signal is selected either by setting both external control signals, MODE and /LED, to high, or by leaving the inputs unconnected, in which case the two pull-up resistors engage. In order to take over control of the LED backlight, MODE has to be set to low. Then, /LED is a low-active signal—that is, a low state switches the LED backlight on. We used the integrated HCT00 logic device (“HCT” being the device family), which hosts four NAND gates and complies with 3.3 V and 5 V logic level standards, thus providing a safe level translation

Measurements

In this section, we present measurements acquired with a photodiode (Thorlabs PDA36A-EC), which was connected to a PC oscilloscope (Pico Technology PicoScope4224). When it was needed, the control signal for the LED backlight was connected to the oscilloscope as well. The amplifier of the photodiode was set to a gain of 30 dB, which provided a high enough bandwidth (785 kHz) to accurately capture the steep slopes of the luminance signal. The photodiode was equipped with a lens (Pentax 50mm-F1.4) and a lens spacer, which allowed for measuring a field of approximately $4 \times 4 \text{ cm}$ at a distance of 70 cm. The luminance was calibrated using a luminance meter (Minolta LS100).

LCD reaction time In order to quantify the LCD reaction time, we measured luminance curves while the screen was changed either between black and white or between two gray pixel values. Additionally, measurements were taken at two different monitor contrast settings. For the evaluated

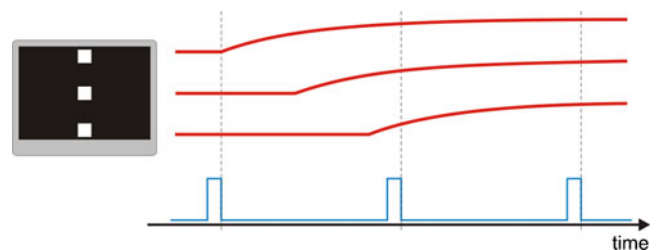


Fig. 4 Illustration of the time shift of the luminance curves (in red) as they would be virtually measured at the top, middle, and bottom of the screen over two full monitor refresh cycles after presenting an image with three patches (as depicted at the left). The vertical synchronization signal (shown at the bottom in blue) marks the start of each update cycle

monitor, the LED backlight was permanently switched on, whereas the other monitor was powered off (Fig. 5).

As can be seen in Fig. 5, several refresh cycles were needed for the pixel values to settle, especially for changes from low to high values. Only in the very special case of switching to the maximum luminance was the reaction time as short as is found in the monitor's specifications (≈ 5 ms). Otherwise—that is, as soon as the contrast setting at the monitor was decreased or a gray-to-gray switch took place—the reaction time increased dramatically; this is the usual case, as the luminance will normally be adjusted by the user during the monitor calibration procedure, either by lowering the contrast setting or by limiting the range of pixel values used in the program.

The reaction times for colored stimuli are the same as for white. This is because white, like any other color that can be presented on the LCD screen, is made of a combination of the three primary colors (i.e., red, green, and blue) created by the colored filters in front of the switching LC pixel cells. Therefore, if white has settled, so have the primary colors.

LED switching characteristics In order to measure the switching characteristics of the tachistoscope in terms of luminance output, a white image was presented on each monitor and calibrated to 100 cd/m^2 . Ideally, it should not make any difference, at least with respect to luminance, whether the backlight is on for Monitor 1 while being off for Monitor 2, or the other way around. That is, the output should always be at 100 cd/m^2 , especially when switching between the backlights. We measured the luminance curves

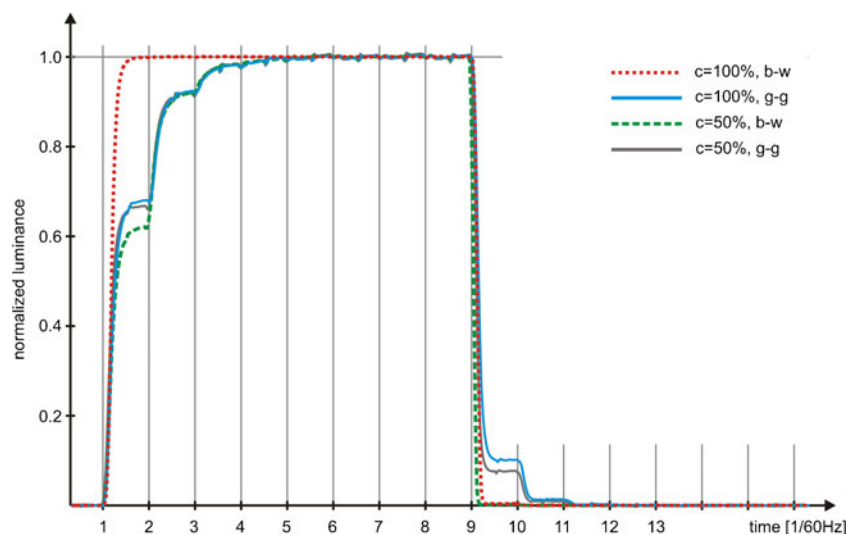


Fig. 5 Normalized luminance curves of a black–white (0 %–100 %) and gray–gray (25 %–75 %) counterphase flicker at different monitor contrast settings (100 % and 50 %). Each phase of the flicker lasted for eight cycles at a 60 Hz refresh rate. Reaction times are only short if the LC cell has to be driven either to “fully closed” or to “fully open.” Note that at a contrast setting of 50 %, the LC cell is never driven “fully

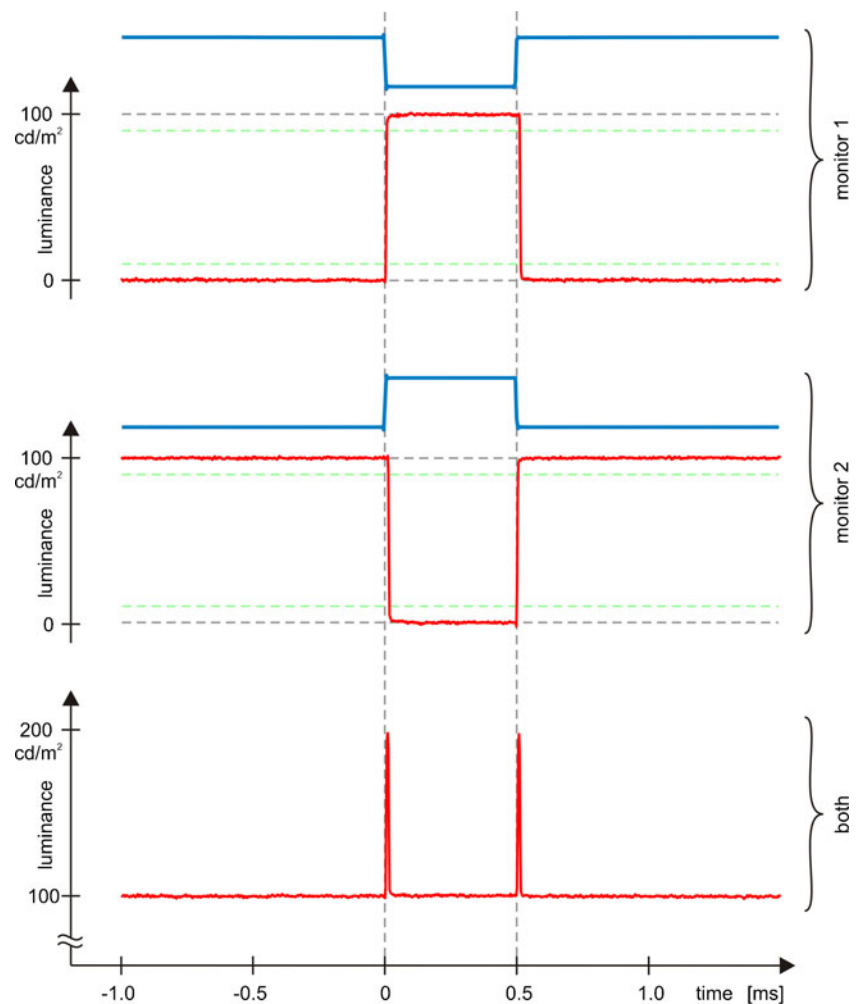
while flashing the backlight of Monitor 1 for $500 \mu\text{s}$. During this flash, the backlight of Monitor 2 was in turn switched off. Control signals for the two monitors were generated by the same parallel port, which allowed for switching both signals in perfect synchrony. Besides measuring the joint luminance output of both monitors, we also measured the luminance contribution of each monitor separately by simply powering off the other monitor (Fig. 6).

As can be seen in Fig. 6, we recorded short pulses of excess light when switching the backlights (see bottom curve). Ideally, this curve would be completely flat. However, small asymmetries in the switching delays cause residual artifacts to show up as glitch pulses. Whether these glitches are tolerable depends on the application at hand and the stimulus durations being used. A compensation circuit can be added to the LED control, which greatly reduces the glitch pulses (see Fig. 7).

As the delay and duration of switching the backlight were of interest, we analyzed the luminance curves that were recorded separately for each monitor. The delay in switching the backlight was defined as the time between the control signal crossing the 50 % threshold and the luminance output changing by 10 % of the final luminance step (i.e., 10 cd/m^2 for a target luminance of 100 cd/m^2). We chose a 10 % threshold instead of a 50 % threshold to minimize contamination of the delay measure by the rise or fall time of the signal. The rise and fall times were defined by the 10 % and 90 % thresholds (shown as horizontal green dashed lines in Fig. 6). Table 1 lists the average delays and rise and fall times, based on ten measurements. As can be seen, the differences in timing

open,” even if the programmed pixel value is 100 %. On the other hand, a pixel value of 0 % is always mapped to a “fully closed” LC cell, irrespective of the contrast setting, which results in a correspondingly quick switch-off time. The curves show averages of five measurement repetitions

Fig. 6 Control signals (blue) and luminance curves (red), as measured while switching the backlights of Monitors 1 and 2 in a complementary fashion; that is, while the backlight of Monitor 1 was switched on for $500\ \mu\text{s}$, the backlight of Monitor 2 was switched off for $500\ \mu\text{s}$. The curves for “Monitor 1” and “Monitor 2” show the light output of each monitor separately; the respective other monitor was powered off during these measurements. On each monitor, a white image calibrated to $100\ \text{cd/m}^2$ was presented. The dashed horizontal lines indicate changes of 0 %, 10 %, 90 %, and 100 % of the complete luminance step, which have been used for the quantitative analysis of the switch timing. The curve at the bottom shows the luminance output when both monitors were powered on



between the two monitors are negligible and well within the expected range of product variability. The within-monitor comparison reveals very similar rise and fall times ($\approx 3\ \mu\text{s}$); however, the delay for switching off the backlight is about $10\ \mu\text{s}$ longer than that for switching it on (e.g., 4.5 vs. $14.4\ \mu\text{s}$ for Monitor 1). This becomes relevant for the compensation circuit described in the next section.

Theoretically, such low timing values suggest stimulus durations potentially as short as $20\ \mu\text{s}$ and stimulus frequencies of $25\ \text{kHz}$ (assuming an on–off ratio of 1). However, although we think that such extreme values can be safely used, we did not test whether this would affect the LEDs and the LED driver. Thus, strictly speaking, only frequencies smaller than the standard PWM frequency, which is around $200\ \text{Hz}$, can be considered safe.

Compensation circuit We measured a longer delay when switching off the backlight as compared to switching it on. This means that stimulus durations were longer than programmed and that a new image (on one monitor) would become visible more quickly than the old image (on the other monitor) would become invisible. However, the

difference in the delays was just $10\ \mu\text{s}$ (Table 1), which, if not tolerable or accounted for otherwise, can easily be compensated for by delaying the LED control signal when the backlight is switched on, but not when it is switched off. To this end, the LED control signal was fed through a small and passive analog compensation circuit (Fig. 7). This circuit decreased the slope just of the falling edge of the signal, and thus increased the time needed for the signal to reach the threshold of digital input at the monitor.

As can be seen in the lower curve of Fig. 8, this compensation circuit makes the glitch pulses disappear almost completely when properly adjusted. However, looking at the joint luminance output for the special case of a white-on-white flash is somewhat misleading, as it hides the rise and fall times of the individual luminance curves; these times are not affected by the compensation circuit, in either a positive or a negative sense. This is due to the digital signal processing at the LED driver input, for which the steepness of the slope of the input signal is irrelevant. Only the time at which the input crosses the threshold matters. Table 2 lists the timing values based on ten measurements with the compensation circuit in place. As can be seen, in comparison to the values measured

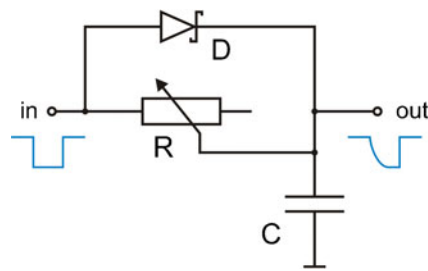


Fig. 7 This circuit allows compensation for the asymmetries in the LED backlight on–off switching delays. The adjustable resistor (R) and the capacitor (C) form a simple RC low-pass filter that decreases the slope of the signal. This filter, however, is only active when the signal changes from high to low; in the opposite direction (i.e., from low to high), the diode (D) basically shorts out the resistor (i.e., $R \approx 0$), which annuls the filter. Increasing the fall time of the negative signal edge increases the switching delay, as it takes longer for the signal to reach the threshold of the digital LED control input. We chose $R = 5 \text{ k}\Omega$, $C = 10 \text{ nF}$, and the Schottky diode BAT42. If a high-active signal is used (i.e., a high level switches on the LED backlight), the polarity of the diode must be reversed

without the compensation circuit (Table 1), only the mean values for the delays differ, whereas rise and fall times remain unchanged.

Luminance stability In a tachistoscope application, the backlight of one monitor is often kept switched on most of the time, whereas the backlight of the other monitor is just flashed briefly from time to time, meaning that the LED and drivers for both monitors operate at different temperatures, possibly causing significant differences in the color and luminance outputs. We measured the luminance output of the LED backlight after a 2-min cool-off phase (Fig. 9). When a cold LED is switched on, it is about 4 % brighter than after warming up. Where necessary, this can be taken into account when calibrating the monitors or by using the monitors along with their backlights in a more balanced way.

Table 1 Means and standard deviations of the backlight switching times (in microseconds) as measured from ten luminance curves for each monitor

	Backlight Switched On		Backlight Switched Off	
	Delay	Rise Time	Delay	Fall Time
Monitor 1				
<i>M</i>	4.5	2.5	14.4	2.8
<i>SD</i>	0.024	0.123	0.068	0.352
Monitor 2				
<i>M</i>	4.6	2.9	14.2	2.7
<i>SD</i>	0.024	0.266	0.015	0.189

The rise and fall times are defined by 10 % and 90 % luminance changes, respectively, where 100 % is the full nominal luminance change. Delays are measured between the LED control signal (50 % signal change at the parallel port output) and a 10 % luminance change

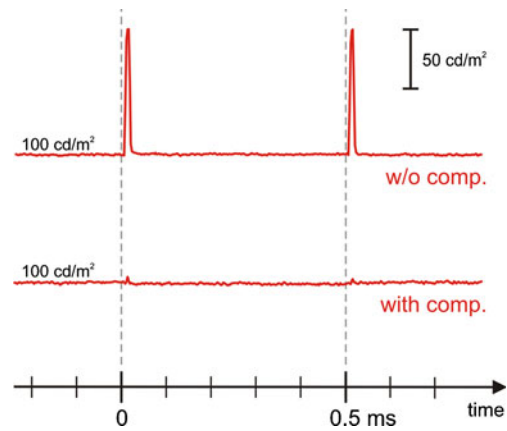


Fig. 8 Luminance curves when flashing a white image on Monitor 1 for $500 \mu\text{s}$ while switching off the white image on Monitor 2 in a complementary fashion. The curve at the top is a close-up of the bottom curve in Fig. 6. The two peaks are artifacts caused by asymmetries in the switching delays. The luminance curve at the bottom was measured under the very same conditions, but with the control signal looped through the compensation circuit shown in Fig. 7 (one per monitor)

In order to evaluate the predictability and stability of the stimulus luminance under more realistic experimental conditions, we measured the relative error in luminous stimulus energy for 20 different stimulus durations between $200 \mu\text{s}$ and 20 ms. The interstimulus intervals were chosen randomly on a logarithmic time scale, between 500 ms and 5 s. For each stimulus presentation, we recorded the LED control signal and the luminance signal, computed the integral of the luminance signal, divided this integral by the expected stimulus energy, and subtracted 1, providing us with the relative error in stimulus energy. We preferred to base the error measure on energy rather than on luminance, because at the short presentation times used here, the visual system is more sensitive to the stimulus energy than to a luminance modulation.

The expected stimulus energy was calculated as the *stimulus duration* multiplied by the *steady-state luminance*, where the steady-state luminance was measured after an LED warm-up phase of 15 s. In our setup, we used a standard PC with a parallel port for generating the LED control signal, which,

Table 2 Means and standard deviations of the backlight switching times (in microseconds) as measured from ten luminance curves for each monitor, with the compensation circuit in place

	Backlight Switched On		Backlight Switched Off	
	Delay	Rise Time	Delay	Fall Time
Monitor 1				
<i>M</i>	15.6	2.6	14.0	2.8
<i>SD</i>	0.037	0.162	0.043	0.183
Monitor 2				
<i>M</i>	15.0	2.8	13.5	2.7
<i>SD</i>	0.026	0.253	0.028	0.243

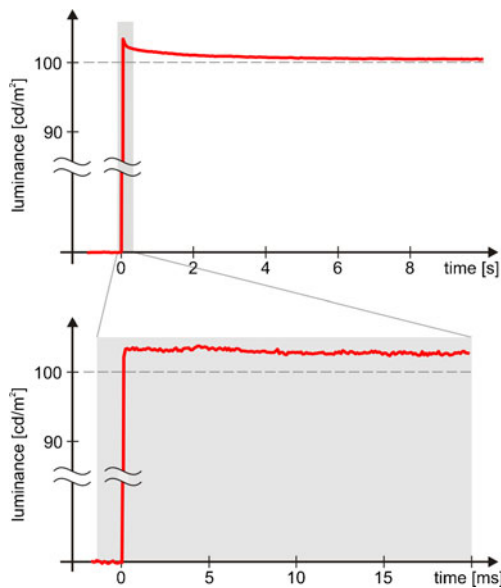


Fig. 9 Luminance output of the LED backlight at different time scales after a 2-min cool-off period. The light output was calibrated to be 100 cd/m^2 after a warm-up phase of several minutes

however, was only accurate to a few microseconds. Therefore, we used the measured width of the LED control signal pulse as the stimulus duration rather than the programmed value when calculating the expected stimulus energy. Moreover, the compensation circuit described earlier (see Fig. 7) was in place during the measurements, which makes a difference especially for very short presentation times. For example, if a programmed 200 μs stimulus turns out to be a mere 10 μs longer because of the differences in the switching delays (see Table 1), this would result in a systematic additional error of $10/200 = 5\%$.

Measurements were repeated in a randomized fashion over 18 min, resulting in about 30 repetitions per tested duration value. Figure 10 shows the averages that were calculated, while pooling data over the randomly chosen interstimulus intervals.

The errors shown in Fig. 10 are all positive: That is, the stimulus energies were systematically higher than the energies

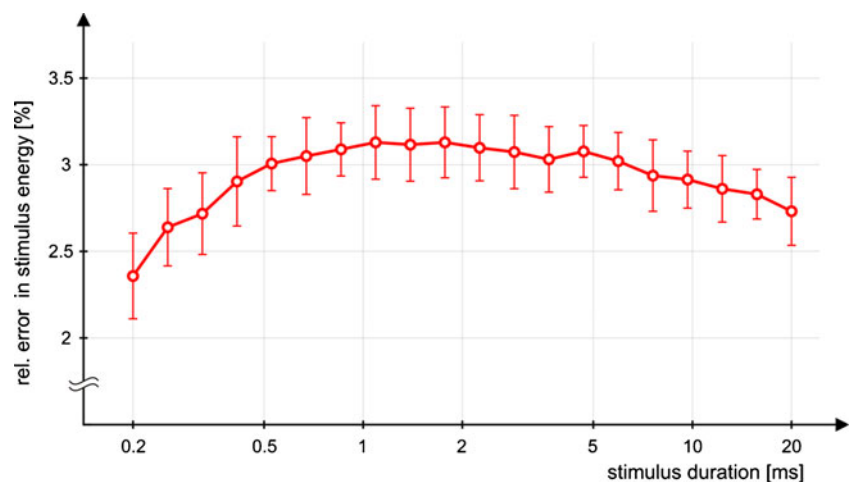
calculated from the respective stimulus duration and the steady-state luminance. This was to be expected, given that the luminous output was found to be higher for cold LEDs (see Fig. 9) and that the LEDs must have been rather cold also during the pulsed stimulus measurements, as they were switched on only once in a while and only for very brief periods of time. The variability of the measured errors—that is, the repeatability error—was nearly independent of the stimulus duration and, overall, very small ($SD_{\text{avg}} = 0.2\%$).

Discussion

Tachistoscopes have been widely used in vision research for experiments necessitating extremely brief visual stimulus presentations. Despite technological improvements made over the years, the available tachistoscopes remain expensive and depend strongly on customized components. Yet exposure times are still limited to the millisecond range, and timing accuracies are comparably low.

Here we have presented an inexpensive two-channel tachistoscope offering exposure durations well below one millisecond at a high precision of timing. We measured rise and fall times of the luminance output of about 3 μs , which allows for extremely short exposure durations. Such short rise and fall times greatly reduce timing uncertainties, not only while switching between the two monitors, but also with respect to the onset and duration of the stimuli. In our application, the precision of stimulus timing was only limited by the PC that controlled the tachistoscope. Despite the short rise and fall times, we found asymmetries in the switching delays of about 10 μs . We showed that these asymmetries, which cause minor switching artifacts, can be minimized by adding a simple compensation circuit to the LED control. Finally, we found the luminance of a cold LED backlight to be about 4% higher than after it warmed up. This bias could be accounted for

Fig. 10 Relative errors in luminous stimulus energy over the stimulus duration. Measurements have been randomized, and each data point represents about 30 measurements for one stimulus duration, which have been averaged irrespective of different interstimulus intervals. The bars indicate the corresponding $\pm SD$ intervals



when calibrating the monitor or by using the two monitors in a way that avoids cooling off the LED backlights. More importantly, we found the repeatability error regarding the stimulus energy to be very low across different stimulus durations ($SD_{\text{avg}} = 0.2\%$).

Other tachistoscopes adopting LCD technology have been proposed recently. Fischmeister et al. (2010) described a three-channel setup based on LCD projectors and LC shutters. LC shutters rely on the same technology as LCDs and have, at least in principle, the same shortcomings. However, the physical dimensions and the sheer number of pixels in an LCD monitor make it much more difficult to achieve fast reaction times in an LCD as compared to a single and comparatively large LC shutter. Nevertheless, the authors measured rise and fall times of approximately 1 ms and 0.25 ms (10 %–90 %), limiting exposure durations to about 2 ms, an order of magnitude longer than is possible with our approach. Moreover, as these LC shutters do not fully block the light when closed, two shutters per projector had to be mounted serially, further increasing the complexity of the setup and adding to the bill of materials. The setup showed a fairly high variance in output luminance, even when exposure time was fixed—which, however, could be attributed to peculiarities of the projector light sources, and might be resolved by using different projectors. Proper selection of the imaging device is also an issue with our setup, because LED backlights might exhibit irregular switching characteristics when they are switched off for extended periods of time (see Appendix A).

Another problem arises from semipermeable mirrors, as they cause color shifts that depend on the angle of light passing through or being reflected by the mirror (see Appendix B). Projector setups are an advantage in this respect, because they allow for the use of smaller mirrors with correspondingly higher optical quality. Moreover, due to the large throw ratio (i.e., the ratio between projection distance and screen width), the range of angles at which the light passes through or is reflected by the mirror is considerably smaller than in our compact LCD monitor setup. Moreover, these angles do not depend on viewing position, because the projection screen scatters the light. Other advantages of projector setups include a potentially high luminance output and a fairly free choice of screen size. Lately, projectors using LEDs as light sources have become available and provide sufficient luminous output power for the screen sizes typically used in visual experiments, especially in functional magnetic resonance imaging (fMRI) environments, where projector setups are commonly used for visual stimulus presentation. Such projectors would be particularly suited for modifications of the LED electronics and to be used in a tachistoscopic setup, much as we did with our standard LCD monitors.

Thurgood et al. (2010) described a one-channel tachistoscope consisting of an LC panel illuminated by a custom-made

LED array, allowing for exposure durations of 1 ms and above. Although the net output luminance was not reported, it can be assumed to be much higher than the luminance output of the off-the-shelf LCD monitors that we used. However, the advantage of higher luminance output comes at the cost of having to build an LED backlight and properly integrating it with an LC panel so as to get a uniformly illuminated screen. More importantly, a one-channel setup limits the scope of application, as it only allows for brief stimulus presentations over a pitch-black background or, vice versa, a pitch-black stimulus over any background. When these limitations do not play a role, our method can be used in a one-monitor setup as well, while being simpler, cheaper, and faster than the setup described by Thurgood et al. Moreover, if the suggested multiplexer circuit is installed, the monitor can be operated in the backlight switching mode or as a standard stimulus screen. Opting for a two-channel solution with a semipermeable mirror, however, adds more flexibility, as it allows for presenting stimuli over any desired background or, alternatively, presenting two independent stimuli (over a pitch-black background), as would be required for visual masking or priming experiments, for example. In two-stimulus paradigms, the high timing resolution provided by LED backlight switching is not only beneficial for defining short exposure durations, but also for having almost unlimited control over stimulus onset times.

The development of a tachistoscope is technically demanding, and none of the available setups is perfect. Nevertheless, our approach is comparatively inexpensive, as it relies on just two standard LCD monitors, a semipermeable mirror, a mounting rack, and a PC. Even though the monitors have to be modified, the modifications can be kept simple and do not require costly hardware. Therefore, our tachistoscope makes a good compromise between what is technically achievable and what is economically reasonable.

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Appendix A: Monitor selection

The Samsung SyncMaster BX2240 monitor was chosen for no particular reason, other than featuring an LED backlight. This monitor employs a TN (*twisted nematic*)-type LC panel, which is cheaper and supposedly has faster reaction times than other panel technologies, such as, for example, IPS (*in-plane switching*) or VA (*vertical alignment*). On the other hand, TN panels exhibit inferior color quality, not only in terms of color resolution, but also in terms of hue and saturation shifts at increasing viewing angles. The latter problem is not necessarily crucial in the tachistoscope

application, for two reasons. First, the observation distance in visual experiments is normally long, and stimuli are often smaller than the screen size would allow for, both implying sufficiently small viewing angles. Second, and more importantly, the semipermeable mirror causes color distortions anyway, which will likely dominate overall color distortions.

One downside of TN panels is their low native color resolution, which usually is only 6 bits per color channel. Monitor manufacturers overcome this limitation by implementing spatial or spatiotemporal dithering techniques (i.e., by applying noise patterns that increase the apparent color resolution through spatial or spatiotemporal averaging). In addition, some graphics cards apply dithering, also to overcome the limited color resolution imposed by the digital transmission of video signals. Having dithering applied, especially if the details are not documented, might be prohibitive for visual experiments in general. In particular, temporal dithering can be ineffective, and can even create artifacts with stimuli being presented as briefly as in usual tachistoscope applications, in which the stimuli are too short to be covered by more than one dither phase. Moreover, controlling the dither phase into which the stimulus falls would be difficult, and this might cause one and the same stimulus to appear slightly differently from trial to trial. On the other hand, whether such minor differences would actually be perceived given the short presentation times is questionable.

As already mentioned, LC panels differ in their reaction times. Although reaction times do not matter for very simple tachistoscope applications, in which enough time can be provided to let the LC pixel states settle before switching on the LED backlight, fast reaction times can still be of benefit when it comes to experiments requiring rapid serial visual presentation. For the same reason, high refresh rates up and beyond 100 Hz are desirable, as are provided by 3-D LCDs (shutter glasses technology). Although other panel technologies are hitting the market (with or without overdrive techniques), the fastest LCDs to date, especially 3-D LCDs, are still equipped with TN panels.

The most crucial selection criterion is whether the driver electronics of the LED backlight are suitable for the described modification. Normally, it should be easy to identify the signal line that carries the PWM signal, disrupt it, and feed it from an external signal source. Problems may be caused, however, by the extreme on–off ratios to be applied in typical tachistoscope applications. The LED driver will not necessarily tolerate receiving an off signal for an extended period of time. Some drivers go into sleep mode if they are not active for longer than a mere 40 ms, and can cause severe artifacts upon wake-up that effectively compromise tachistoscope performance. Unfortunately, there is no way of telling beforehand whether a monitor hosts such a driver, even if the particular monitor type is thought to

handle long off times well. This is not any different with the Samsung SyncMaster BX2240, which is now being manufactured with an updated internal circuit rendering it unusable for the tachistoscope setup. We also observed this LED driver problem with the 3-D monitors BenQ XL2410T and BenQ XL2420T. Recently, we tested the Fujitsu P23T-6 IPS, which also falls asleep, but does so rather slowly and exhibits a tolerable wake-up behavior. Although the timing performance of the Fujitsu P23T-6 IPS is not optimal, it offers the benefit of having an IPS-type LC panel with reasonably fast reaction time. Detailed measurements can be found at <http://display-corner.epfl.ch>.

Appendix B: Practical issues

We had difficulties adjusting the positions of the two screens and the semipermeable mirror so as to perfectly align them. Keeping the positions of two of the elements fixed—for instance, the mirror and one of the screens—leaves 6 deg of freedom for the third element—for instance, the second screen—to be precisely adjusted. For applications, which would require high alignment accuracy, the mounting rack should be equipped with suitable micro adjustments.

As we mentioned in the Discussion, the semipermeable mirror can induce noticeable color shifts, not only depending on whether the light is transmitted (as for one monitor) or reflected (as for the other monitor), but also depending at which angle an optical trace passes through or is reflected by the mirror. The latter issue is especially problematic, as these angles are different for different locations on the screen and also depend on the position of the observer. Moreover, the polarization of the light (i.e., the orientation of the oscillation plane of the light waves) coming from the LCD panels could play a role, as the mirror might perform differently depending on light polarization. Therefore, if it is crucial for the application at hand, local—for instance, pixel-wise—color calibration will have to be applied to perfectly match the white points over all the screen locations and for both monitors.

Adjusting the maximal luminance is not difficult per se, but it must be kept in mind that the semipermeable mirror removes half of the available luminance, at least. In addition, more luminance may be lost due to monitor calibration. For example, the Samsung SyncMaster BX2240 is specified to provide 250 cd/m², which was enough to provide 100 cd/m² per monitor in our tachistoscope setup. Although this is adequate for many psychophysical experiments, higher luminance values would be desirable in tachistoscope applications in which sufficient stimulus energy has to be provided, despite short presentation times.

Practical information can be found at <http://display-corner.epfl.ch>.

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